# **Computing Tropical Prevarieties With Satisfiability Modulo Theories (SMT) Solvers**

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#### Abstract

A novel way to use SMT (Satisfiability Modulo Theories) solvers to compute the tropical prevariety (resp. equilibrium) of a polynomial system is presented. The new method is benchmarked against a naive approach that uses purely polyhedral methods. It turns out that the SMT approach is faster than the polyhedral approach for models that would otherwise take more than one minute to compute, in many cases by a factor of 60 or more, and in the worst case is only slower by a factor of two. Furthermore, the new approach is an anytime algorithm, thus offering a way to compute parts of the solution when the polyhedral approach is infeasible.

#### 1. Introduction

Tropical geometry [1] has been used to find the order of time scales of variables in chemical reaction networks [2] and for model reduction. It has applications in economics and optimizations like network flows and scheduling.

Satisfiability Modulo Theories (SMT) checking [3] is usually built on top of SAT (Boolean satisfiability), which is the first problem that was proved, in the form of 3SAT, to be NP-complete. SMT checking allows one to test a logical formula with unknowns and relations for satisfiability and, if it is so, for an assignment of the unknowns that leads to the formula's satisfiability. SMT checking is used today in verification of computer hardware and software and has advanced much in recent years due to advances in technology and industrial applications [4].

We present a novel approach to use SMT checking to compute the tropical equilibrium (resp. prevariety). We believe this to be of use, since SMT is a very active field of research, yet problems of tropical geometry have not been solved with SMT until now.

In the following, we describe the idea of tropical geometry and SMT in the remainder of this section. In Sect. 2 we describe the exact problem and Sect. 3 describes the proposed solution and several possible improvements. Section 4 has results of speed tests of our implementation SMTcut for various SMT solvers and possible optimizations.

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#### 1.1. Some Tropical Geometry

Given a system of polynomial equations with zero r.h.s., the basic idea is to express its indeterminates  $x_i \in \mathbb{R}_+$  and parameters  $k_\alpha \in \mathbb{R}_+$  as powers of some  $\varepsilon \in (0,1)$  times a value  $\bar{x}_i$  resp.  $\bar{k}_\alpha$  that is roughly 1. That is, indeterminates become  $x_i = \bar{x}_i \varepsilon^{a_i}$  and parameters  $k_\alpha = \bar{k}_\alpha \varepsilon^{\gamma_\alpha}$ , with  $\bar{x}_i \approx 1 \approx \bar{k}_\alpha$ .

Let  $x \in \mathbb{R}^d_+$  and  $\alpha, \beta \in \mathbb{N}^m_0$  be multi-indices with  $x^{\alpha} = \prod_i x_i^{\alpha_i}$ . Furthermore, let  $\mathcal{P}$  and  $\mathcal{N}$  be index sets of the terms with positive resp. negative sign. We write the polynomial equation system as

$$\sum_{\alpha \in \mathcal{P}} k_{\alpha} x^{\alpha} - \sum_{\beta \in \mathcal{N}} k_{\beta} x^{\beta} = 0.$$
 (1)

Next, we sort all terms with positive sign to one side and all terms with negative sign to the other. Hence, the equation becomes

$$\sum_{\alpha \in \mathcal{P}} k_{\alpha} x^{\alpha} = \sum_{\beta \in \mathcal{N}} k_{\beta} x^{\beta}.$$
 (2)

The critical observation is now that on each side almost all of the time one term dominates all others [5]. In tropical geometry we only look at this dominating term. A *tropical root* is found when the dominating terms on both sides cancel each other out. Since  $\varepsilon < 1$ , the inequality  $\bar{x}\varepsilon^a > \bar{x}'\varepsilon^{a'}$  is approximately equivalent to a < a'. "Domination" thus means that a is minimal.

With the above sketched idea of *tropicalization*, we transform equation (2) into its tropical counterpart to look for tropical roots:

$$\min_{\alpha \in \mathcal{P}} \left( \log_{\varepsilon}(k_{\alpha}) + \sum_{i} \alpha_{i} x_{i} \right) = \min_{\beta \in \mathcal{N}} \left( \log_{\varepsilon}(k_{\beta}) + \sum_{i} \beta_{i} x_{i} \right).$$

In order for this equation to hold, the minimum has to be attained at least twice, one time on each side. Observe that the equation consists now only of minima of linear functions and can thus readily be expressed as a set of polyhedra.

One polyhedron is defined by each combination of  $\alpha \in \mathcal{P}$  and  $\beta \in \mathcal{N}$  that yields a hyperplane via

$$\log_{\varepsilon}(k_{\alpha}) + \sum_{i} \alpha_{i} x_{i} = \log_{\varepsilon}(k_{\beta}) + \sum_{i} \beta_{i} x_{i}, \tag{3}$$

while for all  $\eta \in \mathcal{P} \cup \mathcal{N}$  half-spaces are defined by

$$\log_{\varepsilon}(k_{\alpha}) + \sum_{i} \alpha_{i} x_{i} \leq \log_{\varepsilon}(k_{\eta}) + \sum_{i} \eta_{i} x_{i}. \tag{4}$$

A set of polyhedra is defined by cycling over all possible choices for  $\alpha$  and  $\beta$ .

Since a polynomial system may consist of multiple equations, we get multiple sets of polyhedra. Because we are looking for solutions where all polynomials are zero at the same time, all constraints (3) and (4) have to hold at the same time and hence the sets of polyhedra have to be intersected. The resulting set of polyhedra is called a *tropical equilibrium*.

For computations, the parameter  $\varepsilon$  in the above construction has to be provided. Furthermore, the  $\log_{\varepsilon}(k_{\alpha})$  are rounded to rationals. Tropical geometry focuses on the dominant terms and

hence yields only approximate results. The resulting coarse-graining can be helpful to find broad areas where the dominant terms cancel each other out.

Equations like (1) can be used to model chemical reaction networks, where all quantities (concentrations and reaction speeds) are positive values. The resulting matching of positively and negatively signed terms in (2) is called *opposite sign condition*.

If no such distinction is made and all terms—regardless of their sign—can cancel each other out, then a *tropical prevariety* is computed. In the above formalism this can be achieved by defining both  $\mathcal{P}$  and  $\mathcal{N}$  to contain the indices of all terms. The tropical prevariety is a superset of the tropical equilibrium.

We will continue to speak of equilibria, but the presented algorithm works for prevarieties as well, since the difference is only in the input. In Sect. 4 we show run-times only for computations of equilibria, since the inputs for these benchmarks come from chemical reaction networks.

## 1.2. Bringing SMT Into the Picture

The problem that we are solving is the intersection of several unions of polyhedra. That is, given polyhedra  $P_{ij}$  and unions of (convex) polyhedra  $B_i = P_{i1} \cup P_{i2} \cup \ldots \cup P_{in_i}$ , we are interested in the intersection  $\bigcap_i B_i = \{R_1, R_2, \ldots, R_\ell\}$ , where the  $R_i$  are again (convex) polyhedra. In this article we show how to use SMT checking to solve this problem.

Satisfiability Modulo Theories (SMT) checking allows us to decide if a logical formula, with atoms that are themselves equations or inequalities, is satisfiable or not. For example,  $x > 1 \land x < 2$  is such an SMT formula. One has to specify a *theory* of numbers that unknowns in the formula can assume. In the above example, the problem is satisfiable in the theory of real numbers, but not in the theory of integers. If an SMT problem is satisfiable, SMT can return a *model*, which is an assignment for all unknowns in the formula.

SMT solvers may be used in *incremental mode*, where one can add additional *assertions*, i.e., clauses that are combined with AND, and continue to look for further models after one has found a solution. This can save a lot of time and we will make use of it later.

## 2. The Problem

A (convex) polyhedron is defined as the intersection of finitely many hyperplanes and half-spaces. Furthermore, each hyperplane can be expressed as two (closed) half-spaces, thus a polyhedron can be described as a finite number of half-spaces [6].

Given the ambient space  $\mathbb{Q}^d$ , a (closed) half-space H is a set

$$H = \{ \boldsymbol{x} \in \mathbb{Q}^d \mid \lambda_0 + \lambda_1 x_1 + \lambda_2 x_2 + \ldots + \lambda_d x_d \le 0, \lambda_i \in \mathbb{Q} \}.$$
 (5)

Given half-spaces  $H_k$ , we define a polyhedron as

$$P = \bigcap_{k} H_{k}.$$
 (6)

A bag is what we call a union of polyhedra  $P_i$ , i.e.,

$$B = \bigcup_{j} P_{j}.$$

Finally, we are looking for the intersection of said bags  $B_i$ , that is

$$V = \bigcap_{i} B_{i} = \bigcap_{i} \bigcup_{j} P_{ij} = \bigcup_{k} R_{k}. \tag{7}$$

The naive solution to the problem of computing the intersection is to cycle successively through all combinations. To do that, pick two bags  $B_j$  and  $B_{j'}$ ,  $j \neq j'$ , and intersect all polyhedra from one with all polyhedra from the other to form a new bag B'. Then, remove  $B_j$  and  $B_{j'}$  from the set of bags and insert B' instead. Continue this procedure until there is only one bag left, which will then consist of the sought polyhedra  $R_1, R_2, \ldots, R_\ell$ . This is the solution that was used in [2] and, with some refinements, in PtCut [7].

The problem with this solution is that the complexity is exponential in the number of bags. In practice, it often happens that the number of intermediate results, i.e., the number of polyhedra in some B', is very high, even if in the end there are only a few solution polyhedra. This intermediate expression swell makes computing the intersection V infeasible for some models.

Table 2 contains BioModels from our survey and lists their number of resulting polyhedra and maximum number of intermediate polyhedra. Details on the computation can be found in Sect. 4.

## 3. The Procedure

First, we have to formulate our problem as an SMT problem. Fortunately, it is easy to convert a polyhedron as defined in (6) into a logical formula. Set theory maps easily to logical formulas with union mapping to logical OR and intersection to logical AND. In the following,  $\tilde{H}$  denotes the logical formula that defines the set H. Thus, (7) expands to

$$\tilde{V} = \bigwedge_{i} \bigvee_{j} \bigwedge_{k} \tilde{H}_{ijk}$$

and definition (5) of  $H_{ijk}$  employs a linear function that can be used as a formula in SMT. Call the resulting SMT formula f. We can use an SMT solver to decide the satisfiability of f and, what's more important, get an  $x \in \mathbb{Q}^d$  that satisfies the constraints, if there is one.

Next, we look for a matching polyhedron that includes x and is included in the solution V. Since x is contained in the intersection of the  $B_i$ , it must be contained in at least one polyhedron  $P_{ij}$  per bag  $B_i$ . Thus, we cycle through all  $B_i$  to find a containing  $P_{ij}$ , call it  $P'_i$ . (There may be more than one  $P_{ij} \ni x$ , but any will do.)

Obviously, the intersection  $R' = \bigcap_i P'_i$  includes x, but most likely R' has higher dimension than that. Furthermore, since R' is the intersection of exactly one polyhedron per bag it is included in V as well. Hence, we have found a polyhedron that includes x.

In the next step, we modify our initial formula f to exclude the polyhedron R', like this:

$$f' = f \wedge \neg R'$$
.

Notice that we are only adding another assertion to the formula, so we can utilize the incremental mode of SMT solvers to save (a lot of!) time for its next computation.

The important observation here is that we are expanding the original formula f—which describes all solution points—to exclude what we already know to be a solution and continue the search. Thus the procedure generates an ever growing subset of the solution V, making it an anytime algorithm [8]. We can iterate this process until formula f' is unsatisfiable.

This is the algorithm in Python-style pseudocode:

```
# input: a list '11' of sets of polyhedra.
    # output: a list 'rr' of polyhedra.
3
    def compute_polyhedron_dnf(11):
4
        # set the solver to re-use its heuristics
5
        solver = Solver(incremental=True)
        f = convert_to_SMT_formula(11)
7
                             # results list
        rr = []
8
        while True:
9
            # add the formula to the (existing) assertions.
10
            solver.add assertion(f)
11
            # get the model (a variable assignment) that fits the
12
            # constraints, or None if 'f' is unsatisfiable.
13
            x = solver.get_model()
14
            if x is None:
15
                break
                              # formula unsatisfiable
16
            R = []
                             # resulting polyhedron
17
            # cycle through all bags 'B' and
            # collect constraints of polyhedron containing 'x'.
18
19
            \quad \textbf{for} \ B \ \textbf{in} \ 11\colon
20
                 # cycle through all polyhedra 'P' in bag 'B'.
21
                 for P in B:
22
                     if P.contains(x):
23
                         R.append(P.constraints())
24
                         break
25
            # now 'R' defines a polyhedron surely in the intersection.
26
            # exclude 'R' from further searches.
27
            f = Not(R)
                              # new assertion for next round
28
            rr.append(R)
29
        return rr
                              # list of polyhedra.
```

The result of this function is a list of polyhedra. Mathematically, this union of polyhedra describes the equilibrium (resp. prevariety) V. Yet, there are some problems that we address in the next section.

The logic used for SMT formulas is QF\_LRA, that is, quantifier-free linear real arithmetic (here "real" means rational). This allows Boolean propositional logic of equations/inequalities consisting of linear functions over elements of  $\mathbb{Q}$  [9].

#### 3.1. Improvements to the Procedure

#### Non-Maximal Polyhedra

The main issue we experience with the procedure compute\_polyhedron\_dnf is that the polyhedron R computed from point x is often not maximal. That is, R is only a lower dimensional face of a higher-dimensional polyhedron. The full high-dimensional polyhedron will eventually be found by the procedure, but earlier-found lower-dimensional faces would still remain in the result list rr, albeit superfluous.

To avoid this, we test if each newly found polyhedron R is included in one of the already computed polyhedra of result list rr. Unfortunately, this causes quadratic run-time in the

number of resulting polyhedra. But there is an observation that can reduce the constant.

If the newly found polyhedron R is included in some already found polyhedron R', then obviously, point  $x \in R$  is included in R' as well. Testing if a point is included in a polyhedron is simple and fast, so one can test this first. Only if this test succeeds one must perform the full polyhedron inclusion test. Measurements show that with this heuristic, almost all polyhedron inclusion tests can be avoided. See Sect. 4 for details.

In our procedure, we would have to modify function contains in line 22 and function append in line 23 according to these observations.

## **Superfluous Constraints**

Another issue is the redundancy of the constraints that are collected in line 23. Efficiency can be increased by minimizing the set of constraints: the larger the number of constraints, the larger the memory demand and, of course, SMT checking times.

One can simply cycle through all constraints, test if each of them is really required and if not, drop it. The remaining set is not necessarily a minimal set, though.

Here's how this can be done: Let c be the constraint in consideration, g the formula before and  $g' = g \wedge c$  after the addition. If g' is more restrictive than g (i.e., c makes a difference), then the following is unsatisfiable:

$$g \wedge \neg g' = g \wedge \neg (g \wedge c)$$

$$= g \wedge (\neg g \vee \neg c)$$

$$= (g \wedge \neg g) \vee (g \wedge \neg c)$$

$$= g \wedge \neg c.$$

We use SMT checking and apply this formula to all constraints to drop superfluous ones.

#### **Preprocessing**

We explored the possibility to improve the speed of the procedure by preprocessing the input, i.e., the sets of polyhedra.

For one, one can collect all constraints from all bags with only one polyhedron each. Call the resulting polyhedron C. Because of distributivity these constraints hold for all polyhedra of the solution. Hence, we can intersect all polyhedra in their bags with C to test if the intersection is empty, in which case we drop the polyhedron from its bag to reduce computation time.

A more powerful version of this technique can be used to test polyhedra in all bags on if they are required for the definition of the solution in (7). Let B be the polyhedron in question, A the union of all other polyhedra in B's bag and C the intersection of all other bags. Then the solution is  $(A \cup B) \cap C$ . If B is required, then  $A \cap C \neq (A \cup B) \cap C$  and in particular  $A \cap C \subseteq (A \cup B) \cap C$ . Thus, the following set is non-empty:

$$((A \cup B) \cap C) \setminus (A \cap C) = (A \cup B) \cap C \cap \overline{A \cap C}$$
$$= (A \cup B) \cap C \cap (\overline{A} \cup \overline{C})$$
$$= (A \cup B) \cap C \cap \overline{A}$$

$$=B\cap C\cap \overline{A}.$$

This can easily be tested with SMT checking for each polyhedron B per bag and the superfluous polyhedra are dropped, again reducing the computation time.

#### 4. Benchmarks

To benchmark the procedure <code>compute\_polyhedron\_dnf</code>, we created input sets of polyhedra of chemical reaction networks. The reaction networks were taken from the BioModels database [10], which contains models formulated in SBML [11]. The SBML models were converted to ODE systems with polynomial or rational functions using ODEparse [12]. The resulting ODE systems can be downloaded from ODEbase [13] at <a href="http://odebase.cs.uni-bonn.de">http://odebase.cs.uni-bonn.de</a>. If the ODE systems contained rational functions, we multiplied each equation with its common denominator to get a polynomial.

These polynomials were then tropicalized as sketched in Sect. 1.1. The parameter  $\varepsilon$  was set to 1/11 and the logarithms in (3) and (4) were rounded to integers. The sets of polyhedra created by tropicalization were saved with polyhedra expressed as sets of equalities and inequalities.

The software used for polyhedral computation was PtCut 3.5.1 [7] and was run under Windows 10 64-bit using Python 3.7.7. Polyhedral computation were done with the help of the Parma Polyhedra Library (PPL) [14], version 1.2.

The procedure compute\_polyhedron\_dnf was implemented in Python as SMTcut and SMTcut 4.6.4 was used for benchmarking. SMTcut is available under a free software license from https://gitlab.com/cxxl/smtcut.

Neither PtCut nor SMTcut make active use of multithreading. All input and output files are available from https://gitlab.com/cxxl/smtcut\_data\_2 in one large ( $\approx$  42 MiB) repository.

The machine for tests was an Intel Core i7-5820K CPU with 48 GB of memory. We used the solver-agnostic framework PySMT 0.9.0 [15] to access SMT solvers. Of the seven supported solvers, the solvers CUDD, PicoSAT and Boolector could not be used, since they do not support the QF\_LRA logic. This left us with the SMT solvers MathSAT 5.6.1 [16], Z3 4.8.7 [17], CVC4 1.7-prerelease [18] and Yices 2.6.2 [19]. SMTcut was run on Ubuntu Linux 18.04 64-bit with Python 3.7.6.

Table 1 shows a comparison of run-times for all BioModels that completed within two hours, sorted by ascending run-time.

The lowest computation times were achieved with CVC4, if—with the exception of BioModel 183—computation took more than 12 seconds. Below that time Yices was often faster. If we look at run-time per round we see that Yices had always the lowest run-times per round for models that took less than 12 seconds to compute. For unknown reasons, Yices often needs more rounds than other solvers, especially CVC4.

The geometric means of run-times of completed computations for CVC4, Yices, MathSAT and Z3 were 4.93, 5.37, 5.49 and 6.77 seconds, respectively. For that reason, we used CVC4 as solver in further comparisons.

Table 2 shows a comparison of run-times between PtCut and SMTcut with CVC4 as solver. We can make several observations from the data.

**Table 1**Comparison of run-times for different solvers sorted by ascending run-time. The minimal time is printed in bold. Column "BM" contains the BioModel number; "Rounds" is the number of iterations needed to complete the procedure.

397		Run-time [s]				Rounds				Run-time / round [s]			
Column	BM	MSAT	<b>Z</b> 3	CVC4	Yices	MSAT	Z3	CVC4	Yices	MSAT	<b>Z</b> 3	CVC4	Yices
14	397	0.1	0.1	0.1	0.1	1	1	1	1	0.128	0.108	0.147	0.092
30	26	0.1	0.1	0.1	0.1	7	8	8	8	0.016	0.017	0.016	0.012
492         0.3         0.2         0.3         0.2         2         2         2         0.146         0.1120         0.158         0.083           491         0.3         0.2         0.3         0.2         2         2         2         0.146         0.118         0.130         0.084           48         0.8         0.7         0.8         0.4         19         25         21         20         0.028         0.032         0.027         0.020           28         0.6         0.9         0.4         0.5         25         35         20         32         0.022         0.025         0.022         0.012         0.013         0.020           221         0.7         0.8         0.7         0.6         55         58         53         68         0.012         0.014         0.013         0.020           21         0.7         0.9         0.7         0.6         56         65         61         67         0.012         0.015         0.011         0.013         0.022           21         0.7         0.9         0.7         0.6         56         65         61         67         0.012         0.015	41	0.2	0.2	0.2	0.1	7	10	7	8	0.025	0.022	0.030	0.017
491         0.3         0.2         0.3         0.2         2         2         2         0.146         0.118         0.130         0.084           48         0.8         0.7         0.8         0.4         12         13         8         8         0.068         0.05         0.04           482         0.5         0.8         0.6         0.4         19         25         21         20         0.022         0.032         0.027         0.020           28         0.6         0.9         0.4         0.05         25         35         20         32         0.022         0.027         0.03         0.020           21         0.7         0.8         0.7         0.6         55         66         65         61         67         0.012         0.014         0.013         0.009           315         0.8         1.0         0.8         0.8         25         30         19         36         0.011         0.013         0.033         0.041         0.022           328         2.0         2.9         1.7         1.5         93         105         89         90         0.022         0.027         0.011         0.	30	0.2	0.2	0.2	0.2	8	8	7	8	0.026	0.028	0.029	0.020
48         0.8         0.7         0.8         0.4         12         13         8         8         0.068         0.054         0.09         0.44           482         0.5         0.6         0.9         0.4         0.5         25         35         20         32         0.022         0.025         0.022         0.020         0.020         0.020         0.020         0.020         0.020         0.020         0.020         0.020         0.020         0.020         0.021         0.001         0.001         0.002         0.021         0.014         0.013         0.002         0.021         0.07         0.06         55         58         53         68         0.012         0.015         0.011         0.009         0.022         0.027         0.06         55         58         53         68         0.012         0.015         0.011         0.009         0.022         0.027         0.06         55         58         53         68         0.012         0.015         0.011         0.009         0.022         2.02         1.0         1.0         1.0         0.023         0.024         0.033         0.041         0.023         0.041         0.023         0.041         0.023 <td>492</td> <td></td> <td></td> <td></td> <td>0.2</td> <td></td> <td></td> <td></td> <td>2</td> <td>0.141</td> <td>0.120</td> <td>0.158</td> <td></td>	492				0.2				2	0.141	0.120	0.158	
482         0.5         0.8         0.6         0.4         19         25         21         20         0.028         0.032         0.027         0.020           28         0.6         0.9         0.4         0.5         25         35         20         32         0.022         0.027         0.031         0.020           211         0.7         0.8         0.7         0.6         55         58         53         68         0.012         0.014         0.013         0.009           21         0.7         0.9         0.7         0.6         56         65         61         67         0.012         0.015         0.011         0.009           315         0.8         1.0         0.8         0.8         25         30         19         36         0.031         0.033         0.041         0.002           328         2.0         2.9         1.7         1.5         93         105         89         90         0.022         0.027         0.019         0.017           200         2.0         1.9         2.2         1.6         1.7         48         48         36         52         0.043         0.048	491	0.3	0.2	0.3	0.2	2	2	2	2	0.146	0.118	0.130	0.084
28         0.6         0.9         0.4         0.5         25         35         20         32         0.022         0.025         0.022         0.011           637         0.6         0.7         0.6         55         58         53         68         0.012         0.014         0.013         0.009           21         0.7         0.9         0.7         0.6         55         58         53         68         0.012         0.015         0.011         0.009           315         0.8         1.0         0.8         0.8         2.5         30         19         36         0.031         0.033         0.041         0.022           328         2.0         2.9         1.7         1.5         93         105         88         90         0.027         0.019         0.017         0.019         0.017         0.00         0.023         0.027         0.019         0.017         0.00         0.023         0.048         0.063         0.035         0.02         2.0         1.1         1.6         38         41         34         45         0.053         0.048         0.063         0.033           22         2.2         3.5	48	0.8	0.7	0.8	0.4	12	13	8	8	0.068	0.054	0.096	0.044
637         0.6         0.7         0.6         0.5         21         27         19         24         0.026         0.027         0.031         0.020           221         0.7         0.8         0.7         0.6         55         58         53         68         0.012         0.014         0.013         0.009           315         0.8         1.0         0.8         0.8         25         30         19         36         0.031         0.033         0.041         0.022           328         2.0         2.9         1.7         1.5         93         105         89         90         0.022         0.027         0.019         0.017           200         2.0         1.9         2.2         1.6         38         41         34         45         0.053         0.048         0.063         0.033           5599         2.1         2.3         1.6         1.7         48         48         36         52         0.043         0.048         0.063         0.033           222         2.2         3.5         1.8         2.3         199         235         165         259         0.011         0.015         0.011	482	0.5	0.8	0.6	0.4	19	25	21	20	0.028	0.032	0.027	0.020
221         0.7         0.8         0.7         0.6         55         58         53         68         0.012         0.014         0.013         0.009           21         0.7         0.9         0.7         0.6         56         65         61         67         0.012         0.015         0.011         0.009           315         0.8         1.0         0.8         0.8         2.5         30         19         36         0.031         0.033         0.041         0.022           328         2.0         2.9         1.7         1.5         93         105         89         90         0.022         0.019         0.017           200         2.0         1.9         2.2         1.6         38         41         34         45         0.053         0.048         0.065         0.035           599         2.1         2.3         1.6         1.7         48         48         36         52         0.043         0.048         0.045         0.033           222         2.2         3.3         1.8         2.3         199         235         165         259         0.011         0.011         0.009	28	0.6	0.9	0.4	0.5	25	35		32	0.022	0.025	0.022	0.017
21         0.7         0.9         0.7         0.6         56         65         61         67         0.012         0.015         0.011         0.009           315         0.8         1.0         0.8         0.8         25         30         19         36         0.031         0.033         0.041         0.022           328         2.0         2.9         1.7         1.5         93         105         89         90         0.022         0.027         0.019         0.017           200         2.0         1.9         2.2         1.6         38         41         34         45         0.053         0.048         0.045         0.033           599         2.1         2.3         1.6         1.7         48         48         36         52         0.043         0.048         0.045         0.033           22         2.2         3.5         1.8         2.3         199         235         165         259         0.011         0.015         0.011         0.009           666         2.7         3.0         2.2         2.6         93         85         85         111         0.029         0.023	637	0.6	0.7	0.6	0.5	21	27	19	24	0.026	0.027	0.031	0.020
315         0.8         1.0         0.8         0.8         25         30         19         36         0.031         0.033         0.041         0.022           328         2.0         2.9         1.7         1.5         93         105         89         90         0.022         0.077         0.019         0.017           200         2.0         1.9         2.2         1.6         38         41         34         45         0.053         0.048         0.063         0.035           599         2.1         2.3         1.6         1.7         48         48         36         52         0.043         0.048         0.045         0.033           22         2.2         3.5         1.8         2.3         199         235         165         259         0.011         0.015         0.011         0.009           666         2.7         3.0         2.2         2.6         93         85         85         111         0.023         0.024         0.023           222         3.2         4.0         3.1         2.3         246         257         228         230         0.013         0.016         0.014	221	0.7	0.8	0.7	0.6	55	58	53	68	0.012	0.014	0.013	0.009
328         2.0         2.9         1.7         1.5         93         105         89         90         0.022         0.027         0.019         0.017           200         2.0         1.9         2.2         1.6         38         41         34         45         0.053         0.048         0.063         0.035           599         2.1         2.3         1.6         1.7         48         48         36         52         0.043         0.048         0.045         0.033           22         2.2         3.5         1.8         2.3         199         235         165         259         0.011         0.015         0.011         0.009           666         2.7         3.0         2.2         2.6         93         85         85         111         0.029         0.038         0.026         0.023           222         3.2         4.0         3.1         2.3         246         257         228         230         0.013         0.016         0.014         0.010           489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.060         0.061 </td <td>21</td> <td>0.7</td> <td>0.9</td> <td>0.7</td> <td>0.6</td> <td>56</td> <td>65</td> <td>61</td> <td>67</td> <td>0.012</td> <td>0.015</td> <td>0.011</td> <td>0.009</td>	21	0.7	0.9	0.7	0.6	56	65	61	67	0.012	0.015	0.011	0.009
200         2.0         1.9         2.2         1.6         38         41         34         45         0.053         0.048         0.063         0.033           599         2.1         2.3         1.6         1.7         48         48         36         52         0.043         0.048         0.045         0.033           22         2.2         3.5         1.8         2.3         199         235         165         259         0.011         0.015         0.011         0.009           666         2.7         3.0         2.2         2.6         93         85         85         111         0.029         0.038         0.026         0.023           222         3.2         4.0         3.1         2.3         246         257         228         230         0.013         0.016         0.014         0.010           638         2.6         2.9         3.2         2.4         37         46         29         51         0.071         0.062         0.019         0.047           489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.044	315	0.8	1.0	0.8	0.8	25	30	19	36	0.031	0.033	0.041	0.022
599         2.1         2.3         1.6         1.7         48         48         36         52         0.043         0.048         0.045         0.033           22         2.2         3.5         1.8         2.3         199         235         165         259         0.011         0.015         0.011         0.009           666         2.7         3.0         2.2         2.6         93         85         85         111         0.029         0.038         0.026         0.023           222         3.2         4.0         3.1         2.3         246         257         228         230         0.013         0.016         0.014         0.010           638         2.6         2.9         3.2         2.4         37         46         29         51         0.071         0.062         0.109         0.047           489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.060         0.061         0.046           365         4.6         5.1         4.3         3.6         80         82         74         82         0.058         0.062         0.059 <td>328</td> <td>2.0</td> <td>2.9</td> <td>1.7</td> <td>1.5</td> <td>93</td> <td>105</td> <td>89</td> <td>90</td> <td>0.022</td> <td>0.027</td> <td>0.019</td> <td>0.017</td>	328	2.0	2.9	1.7	1.5	93	105	89	90	0.022	0.027	0.019	0.017
22         2.2         3.5         1.8         2.3         199         235         165         259         0.011         0.015         0.011         0.009           666         2.7         3.0         2.2         2.6         93         85         85         111         0.029         0.038         0.026         0.023           222         3.2         4.0         3.1         2.3         246         257         228         230         0.013         0.016         0.014         0.010           638         2.6         2.9         3.2         2.4         37         46         29         51         0.071         0.062         0.109         0.047           489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.060         0.061         0.046           365         4.6         5.1         4.3         3.6         80         82         74         82         0.058         0.062         0.059         0.044           396         3.9         4.8         4.2         5.0         75         82         86         121         0.053         0.059         0.044 </td <td>200</td> <td>2.0</td> <td>1.9</td> <td>2.2</td> <td>1.6</td> <td>38</td> <td>41</td> <td>34</td> <td>45</td> <td>0.053</td> <td>0.048</td> <td>0.063</td> <td>0.035</td>	200	2.0	1.9	2.2	1.6	38	41	34	45	0.053	0.048	0.063	0.035
666         2.7         3.0         2.2         2.6         93         85         85         111         0.029         0.038         0.026         0.023           222         3.2         4.0         3.1         2.3         246         257         228         230         0.013         0.016         0.014         0.010           638         2.6         2.9         3.2         2.4         37         46         29         51         0.071         0.062         0.109         0.047           489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.060         0.061         0.046           365         4.6         5.1         4.3         3.6         80         82         74         82         0.058         0.062         0.059         0.044           396         3.9         4.8         4.2         5.0         75         82         86         121         0.053         0.059         0.049         0.041           147         4.1         6.0         4.4         4.0         84         125         90         117         0.048         0.049         0.052 <td>599</td> <td>2.1</td> <td>2.3</td> <td>1.6</td> <td>1.7</td> <td>48</td> <td>48</td> <td>36</td> <td>52</td> <td>0.043</td> <td>0.048</td> <td>0.045</td> <td>0.033</td>	599	2.1	2.3	1.6	1.7	48	48	36	52	0.043	0.048	0.045	0.033
222         3.2         4.0         3.1         2.3         246         257         228         230         0.013         0.016         0.014         0.010           638         2.6         2.9         3.2         2.4         37         46         29         51         0.071         0.062         0.109         0.047           489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.060         0.061         0.046           365         4.6         5.1         4.3         3.6         80         82         74         82         0.058         0.062         0.059         0.044           396         3.9         4.8         4.2         5.0         75         82         86         121         0.053         0.059         0.049         0.043           147         4.1         6.0         4.4         4.0         84         125         90         117         0.048         0.049         0.052         0.038           230         5.5         7.0         5.1         6.3         115         143         99         139         0.048         0.049         0.052<	22	2.2	3.5	1.8	2.3	199	235	165	259	0.011	0.015	0.011	0.009
638         2.6         2.9         3.2         2.4         37         46         29         51         0.071         0.062         0.109         0.047           489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.060         0.061         0.046           365         4.6         5.1         4.3         3.6         80         82         74         82         0.058         0.062         0.059         0.044           396         3.9         4.8         4.2         5.0         75         82         86         121         0.053         0.059         0.049         0.041           147         4.1         6.0         5.1         5.3         115         143         99         139         0.048         0.049         0.052         0.038           498         6.5         9.1         6.1         6.9         231         285         242         333         0.028         0.025         0.021           431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.036         0.03	666	2.7	3.0	2.2	2.6	93	85	85	111	0.029	0.038	0.026	0.023
489         4.3         4.9         3.0         2.5         72         82         49         54         0.059         0.060         0.061         0.046           365         4.6         5.1         4.3         3.6         80         82         74         82         0.058         0.062         0.059         0.044           396         3.9         4.8         4.2         5.0         75         82         86         121         0.053         0.059         0.049         0.041           147         4.1         6.0         4.4         4.0         84         125         90         117         0.049         0.048         0.049         0.035           230         5.5         7.0         5.1         5.3         115         143         99         139         0.048         0.049         0.025         0.038           498         6.5         9.1         6.1         6.9         231         285         242         333         0.028         0.032         0.025         0.021           431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.	222	3.2	4.0	3.1	2.3	246	257	228	230	0.013	0.016	0.014	0.010
365         4.6         5.1         4.3         3.6         80         82         74         82         0.058         0.062         0.059         0.044           396         3.9         4.8         4.2         5.0         75         82         86         121         0.053         0.059         0.049         0.041           147         4.1         6.0         4.4         4.0         84         125         90         117         0.049         0.048         0.049         0.035           230         5.5         7.0         5.1         5.3         115         143         99         139         0.048         0.049         0.052         0.038           498         6.5         9.1         6.1         6.9         231         285         242         333         0.028         0.032         0.025         0.021           431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.036         0.031           102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.036	638	2.6	2.9	3.2	2.4	37	46	29	51	0.071	0.062	0.109	0.047
396         3.9         4.8         4.2         5.0         75         82         86         121         0.053         0.059         0.049         0.041           147         4.1         6.0         4.4         4.0         84         125         90         117         0.049         0.048         0.049         0.035           230         5.5         7.0         5.1         5.3         115         143         99         139         0.048         0.049         0.052         0.038           498         6.5         9.1         6.1         6.9         231         285         242         333         0.028         0.032         0.025         0.021           431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.036         0.030           105         9.6         9.4         9.7         6.7         141         153         143         152         0.068         0.061         0.068         0.044           102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.060	489	4.3	4.9	3.0	2.5	72	82	49	54	0.059	0.060	0.061	0.046
147         4.1         6.0         4.4         4.0         84         125         90         117         0.049         0.048         0.049         0.035           230         5.5         7.0         5.1         5.3         115         143         99         139         0.048         0.049         0.052         0.038           498         6.5         9.1         6.1         6.9         231         285         242         333         0.028         0.032         0.025         0.021           431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.036         0.030           105         9.6         9.4         9.7         6.7         141         153         143         152         0.068         0.061         0.068         0.044           102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.036         0.031         0.024           32         22.0         23.1         12.8         23.5         418         388         282         504         0.053         0.060 </td <td>365</td> <td>4.6</td> <td>5.1</td> <td>4.3</td> <td>3.6</td> <td>80</td> <td>82</td> <td>74</td> <td>82</td> <td>0.058</td> <td>0.062</td> <td>0.059</td> <td>0.044</td>	365	4.6	5.1	4.3	3.6	80	82	74	82	0.058	0.062	0.059	0.044
230         5.5         7.0         5.1         5.3         115         143         99         139         0.048         0.049         0.052         0.038           498         6.5         9.1         6.1         6.9         231         285         242         333         0.028         0.032         0.025         0.021           431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.036         0.030           105         9.6         9.4         9.7         6.7         141         153         143         152         0.068         0.061         0.068         0.044           102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.036         0.031         0.024           32         22.0         23.1         12.8         23.5         418         388         282         504         0.053         0.060         0.046         0.047           407         20.7         30.2         15.7         55.0         307         389         261         881         0.067         0	396	3.9	4.8	4.2	5.0	75	82	86	121	0.053	0.059	0.049	0.041
498         6.5         9.1         6.1         6.9         231         285         242         333         0.028         0.032         0.025         0.021           431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.036         0.030           105         9.6         9.4         9.7         6.7         141         153         143         152         0.068         0.061         0.068         0.044           102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.036         0.031         0.024           32         22.0         23.1         12.8         23.5         418         388         282         504         0.053         0.060         0.046         0.047           407         20.7         30.2         15.7         55.0         307         389         261         881         0.067         0.078         0.060         0.062           477         42.0         72.0         33.8         49.3         793         940         745         1051         0.053	147	4.1	6.0	4.4	4.0	84	125	90	117	0.049	0.048	0.049	0.035
431         7.7         9.7         6.6         7.4         199         224         183         243         0.039         0.043         0.036         0.030           105         9.6         9.4         9.7         6.7         141         153         143         152         0.068         0.061         0.068         0.044           102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.036         0.031         0.024           32         22.0         23.1         12.8         23.5         418         388         282         504         0.053         0.060         0.046         0.047           407         20.7         30.2         15.7         55.0         307         389         261         881         0.067         0.078         0.060         0.062           477         42.0         72.0         33.8         49.3         793         940         745         1051         0.053         0.077         0.045         0.047           576         55.1         78.0         48.6         62.9         838         1064         881         1076         0.066	230	5.5	7.0	5.1	5.3	115	143	99	139	0.048	0.049	0.052	0.038
105         9.6         9.4         9.7         6.7         141         153         143         152         0.068         0.061         0.068         0.044           102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.036         0.031         0.024           32         22.0         23.1         12.8         23.5         418         388         282         504         0.053         0.060         0.046         0.047           407         20.7         30.2         15.7         55.0         307         389         261         881         0.067         0.078         0.060         0.062           477         42.0         72.0         33.8         49.3         793         940         745         1051         0.053         0.077         0.045         0.047           576         55.1         78.0         48.6         62.9         838         1064         881         1076         0.066         0.073         0.055         0.058           93         124.4         121.0         55.3         139.7         1390         1345         870         1865         0.0	498	6.5	9.1	6.1	6.9	231	285	242	333	0.028	0.032	0.025	0.021
102         14.8         19.1         12.2         11.8         399         538         395         497         0.037         0.036         0.031         0.024           32         22.0         23.1         12.8         23.5         418         388         282         504         0.053         0.060         0.046         0.047           407         20.7         30.2         15.7         55.0         307         389         261         881         0.067         0.078         0.060         0.062           477         42.0         72.0         33.8         49.3         793         940         745         1051         0.053         0.077         0.045         0.047           576         55.1         78.0         48.6         62.9         838         1064         881         1076         0.066         0.073         0.055         0.058           93         124.4         121.0         55.3         139.7         1390         1345         870         1865         0.090         0.090         0.064         0.075           183         69.8         132.0         77.7         115.1         29         194         14         284 <td< td=""><td>431</td><td>7.7</td><td>9.7</td><td>6.6</td><td>7.4</td><td>199</td><td>224</td><td>183</td><td>243</td><td>0.039</td><td>0.043</td><td>0.036</td><td>0.030</td></td<>	431	7.7	9.7	6.6	7.4	199	224	183	243	0.039	0.043	0.036	0.030
32         22.0         23.1         12.8         23.5         418         388         282         504         0.053         0.060         0.046         0.047           407         20.7         30.2         15.7         55.0         307         389         261         881         0.067         0.078         0.060         0.062           477         42.0         72.0         33.8         49.3         793         940         745         1051         0.053         0.077         0.045         0.047           576         55.1         78.0         48.6         62.9         838         1064         881         1076         0.066         0.073         0.055         0.058           93         124.4         121.0         55.3         139.7         1390         1345         870         1865         0.090         0.090         0.064         0.075           183         69.8         132.0         77.7         115.1         29         194         14         284         2.408         0.681         5.551         0.405           501         116.1         192.2         102.8         352.5         1018         1516         1045         2819	105	9.6	9.4	9.7	6.7	141	153	143	152	0.068	0.061	0.068	0.044
407         20.7         30.2         15.7         55.0         307         389         261         881         0.067         0.078         0.060         0.062           477         42.0         72.0         33.8         49.3         793         940         745         1051         0.053         0.077         0.045         0.047           576         55.1         78.0         48.6         62.9         838         1064         881         1076         0.066         0.073         0.055         0.058           93         124.4         121.0         55.3         139.7         1390         1345         870         1865         0.090         0.090         0.064         0.075           183         69.8         132.0         77.7         115.1         29         194         14         284         2.408         0.681         5.551         0.405           501         116.1         192.2         102.8         352.5         1018         1516         1045         2819         0.114         0.127         0.098         0.125           430         209.8         196.2         128.2         405.5         2321         2448         2142         4798	102	14.8	19.1	12.2	11.8	399	538	395	497	0.037	0.036	0.031	0.024
477         42.0         72.0         33.8         49.3         793         940         745         1051         0.053         0.077         0.045         0.047           576         55.1         78.0         48.6         62.9         838         1064         881         1076         0.066         0.073         0.055         0.058           93         124.4         121.0         55.3         139.7         1390         1345         870         1865         0.090         0.090         0.064         0.075           183         69.8         132.0         77.7         115.1         29         194         14         284         2.408         0.681         5.551         0.405           501         116.1         192.2         102.8         352.5         1018         1516         1045         2819         0.114         0.127         0.098         0.125           430         209.8         196.2         128.2         405.5         2321         2448         2142         4798         0.090         0.080         0.060         0.085           103         231.0         449.2         224.9         337.2         2781         3072         2609	32	22.0	23.1	12.8	23.5	418	388	282	504	0.053	0.060	0.046	0.047
576         55.1         78.0         48.6         62.9         838         1064         881         1076         0.066         0.073         0.055         0.058           93         124.4         121.0         55.3         139.7         1390         1345         870         1865         0.090         0.090         0.064         0.075           183         69.8         132.0         77.7         115.1         29         194         14         284         2.408         0.681         5.551         0.405           501         116.1         192.2         102.8         352.5         1018         1516         1045         2819         0.114         0.127         0.098         0.125           430         209.8         196.2         128.2         405.5         2321         2448         2142         4798         0.090         0.080         0.060         0.085           103         231.0         449.2         224.9         337.2         2781         3072         2609         2923         0.083         0.146         0.086         0.115           74         1165.6         1118.5         941.5         1694.2         14227         13352         23245 </td <td>407</td> <td>20.7</td> <td>30.2</td> <td>15.7</td> <td>55.0</td> <td>307</td> <td>389</td> <td>261</td> <td>881</td> <td>0.067</td> <td>0.078</td> <td>0.060</td> <td>0.062</td>	407	20.7	30.2	15.7	55.0	307	389	261	881	0.067	0.078	0.060	0.062
93         124.4         121.0         55.3         139.7         1390         1345         870         1865         0.090         0.090         0.064         0.075           183         69.8         132.0         77.7         115.1         29         194         14         284         2.408         0.681         5.551         0.405           501         116.1         192.2         102.8         352.5         1018         1516         1045         2819         0.114         0.127         0.098         0.125           430         209.8         196.2         128.2         405.5         2321         2448         2142         4798         0.090         0.080         0.060         0.085           103         231.0         449.2         224.9         337.2         2781         3072         2609         2923         0.083         0.146         0.086         0.115           74         1165.6         1118.5         941.5         1694.2         14227         13352         13352         23245         0.082         0.096         0.071         0.073           73         1087.1         1647.9         1067.7         1485.4         14977         16294	477	42.0	72.0	33.8	49.3	793	940	745	1051	0.053	0.077	0.045	0.047
183         69.8         132.0         77.7         115.1         29         194         14         284         2.408         0.681         5.551         0.405           501         116.1         192.2         102.8         352.5         1018         1516         1045         2819         0.114         0.127         0.098         0.125           430         209.8         196.2         128.2         405.5         2321         2448         2142         4798         0.090         0.080         0.060         0.085           103         231.0         449.2         224.9         337.2         2781         3072         2609         2923         0.083         0.146         0.086         0.115           74         1165.6         1118.5         941.5         1694.2         14227         13352         13352         23245         0.082         0.096         0.071         0.073           73         1087.1         1647.9         1067.7         1485.4         14977         16294         15522         21118         0.073         0.101         0.069         0.070	576	55.1	78.0	48.6	62.9	838	1064	881	1076	0.066	0.073	0.055	0.058
501         116.1         192.2         102.8         352.5         1018         1516         1045         2819         0.114         0.127         0.098         0.125           430         209.8         196.2         128.2         405.5         2321         2448         2142         4798         0.090         0.080         0.060         0.085           103         231.0         449.2         224.9         337.2         2781         3072         2609         2923         0.083         0.146         0.086         0.115           74         1165.6         1118.5         941.5         1694.2         14227         13352         13352         23245         0.082         0.096         0.071         0.073           73         1087.1         1647.9         1067.7         1485.4         14977         16294         15522         21118         0.073         0.101         0.069         0.070	93	124.4	121.0	55.3	139.7	1390	1345	870	1865	0.090	0.090	0.064	0.075
430         209.8         196.2         128.2         405.5         2321         2448         2142         4798         0.090         0.080         0.060         0.085           103         231.0         449.2         224.9         337.2         2781         3072         2609         2923         0.083         0.146         0.086         0.115           74         1165.6         1118.5         941.5         1694.2         14227         13352         13352         23245         0.082         0.096         0.071         0.073           73         1087.1         1647.9         1067.7         1485.4         14977         16294         15522         21118         0.073         0.101         0.069         0.070	183	69.8	132.0	77.7	115.1	29	194	14	284	2.408	0.681	5.551	0.405
103     231.0     449.2     224.9     337.2     2781     3072     2609     2923     0.083     0.146     0.086     0.115       74     1165.6     1118.5     941.5     1694.2     14227     13352     13352     23245     0.082     0.096     0.071     0.073       73     1087.1     1647.9     1067.7     1485.4     14977     16294     15522     21118     0.073     0.101     0.069     0.070	501	116.1	192.2	102.8	352.5	1018	1516	1045	2819	0.114	0.127	0.098	0.125
74     1165.6     1118.5     941.5     1694.2     14227     13352     13352     23245     0.082     0.096     0.071     0.073       73     1087.1     1647.9     1067.7     1485.4     14977     16294     15522     21118     0.073     0.101     0.069     0.070	430	209.8	196.2	128.2	405.5	2321	2448	2142	4798	0.090	0.080	0.060	0.085
73   1087.1   1647.9   <b>1067.7</b>   1485.4   <b>14977</b>   16294   15522   21118   0.073   0.101   <b>0.069</b>   0.070	103	231.0	449.2	224.9	337.2	2781	3072	2609	2923	0.083	0.146	0.086	0.115
73   1087.1   1647.9   <b>1067.7</b>   1485.4   <b>14977</b>   16294   15522   21118   0.073   0.101   <b>0.069</b>   0.070	74	1165.6	1118.5	941.5	1694.2	14227	13352	13352	23245	0.082	0.096	0.071	0.073
	73				1485.4					0.073	0.101		0.070
5. 55.6., 155 1001.0 110/11 12501 15520 12710 210/0 0.242 0.250 0.174	61	3045.7	4084.1	1661.3	4187.1	12564	16326	12915	24078	0.242	0.250	0.129	0.174

- BioModels 14, 151, 410, 560 and 730: each of them could not be computed with PtCut and it is likely infeasible to do so. SMTcut was at least able to compute part of the solution, even though it is unknown how large a part of the full solution this constitutes.
- BioModels 183 and 491, 492: Here SMTcut was able to play out its full potential: with only one polyhedron in the solution, it took only some rounds until the maximal polyhedron was found. On the other hand, the computation of BioModel 183 with PtCut was

terminated after 20 hours of work with an intermediate number of 15000 polyhedra and still only 5 of 65 iterations done.

- BioModel 397 does not have a solution at all. SMTcut find this in 0.1 s, whereas PtCut takes almost 15 s.
- BioModels 73, 74, 93, 105, 183, 365, 397, 407, 491, and 501: computation time of SMTcut was at least 60 times lower than with PtCut.
- BioModels 102, 328, 430 and 498: here PtCut was up to 2 times faster than SMTcut. The reason is that for models of dimension less than 20 and with many polyhedra, PtCut can be faster if the intermediate expression swell is not too large.
- In this overview, SMTcut was the better choice in all cases where PtCut needed more than 58 s of computation time, and SMTcut never took more than twice the time as PtCut.

## 4.1. Benchmarks of Preprocessing

Table 3 shows a comparison of times with and without preprocessing the input. We make the following observations:

- The computation for BioModel 183 took almost one hour to preprocess. This is due to the extraordinary number of polyhedra in some input bags.
- Taking the time for preprocessing into account, models with more than 800 polyhedra as solution—with the exception of BioModel 103—gained a moderate speed-up (4%–18%) through preprocessing.
- Preprocessing increased the overall run-time for all models with less than 400 polyhedra as solution, sometimes by a factor of 10 or more.

#### 4.2. Profiling of the Different Parts

The relative time needed in different parts of the procedure to compute the whole solution varies with the number of resulting polyhedra. Table 4 shows the relative time spent in three different parts of the procedure:

- S: Searching for another point outside the already known polyhedra,
- M: Minimizing the found polyhedron,
- I: Inserting that polyhedron into the list of already known ones and testing for inclusion.

From the numbers it is obvious that the inclusion check time takes relatively more time as the number of polyhedra grows.

In contrast, SMT checking for every next point needs relatively less time as the number of polyhedra grows and the time needed for minimization is slowly getting less prominent as well.

It looks like the quadratic time inclusion check is the limiting factor for models with many polyhedra.

## Some Profiling of Polyhedral Inclusion Testing

As was described in Sect. 3, the test for inclusion of a newly found polyhedron in the set of already found ones can be sped up by testing containment of the included point x which was found by the SMT solver.

Some cursory investigation shows that the number of full checks that still have to be done over the course of the whole computation is about 0.26–0.68 times the number of polyhedra in the solution.

Yet, even though the constant is low, the run-time of the inclusion test is quadratic and it becomes the most dominant part of the computation for large result lists.

#### 5. Conclusion

We presented a novel method to compute tropical equilibria (resp. prevarieties) from an input of sets of polyhedra. We sketched an algorithm for that purpose and discussed several possible improvements. Furthermore, we ran extensive benchmarks with different SMT solvers to compute equilibria of tropicalizations of 46 different BioModels.

The conclusion is that the novel method is working and its computation times compare favorably with a known algorithm using purely polyhedral methods. The run-times were always smaller for problems that would otherwise take more than 58 seconds to compute, sometimes by a factor of 60 or more. The novel method has also the advantage to be an anytime algorithm, hence it computes more parts of the solution given more time or computation power. This is of importance if computation of the entirety of the solution is infeasible.

The CVC4 SMT solver was overall the fastest solver in this application, yet Yices outperformed CVC4 for models that could be solved in less than 12 seconds.

Preprocessing the input yielded only moderate speed-ups and only on models that had more than 800 polyhedra as solution. Conversely, preprocessing was always more costly for models with less than 400 polyhedra.

### 5.1. Future Work

There is obvious potential for a parallel implementation of the procedure. We should expect an almost linear speed-up.

The rising percentage of time spent checking for inclusion of already known polyhedra should be addressed. If one could assign one-dimensional properties (like dimension) to polyhedra, only parts of the list of already known polyhedra would have to be checked for inclusion.

The computation of non-maximal polyhedra should be avoided. Hence a good and fast heuristic for choosing the  $P'_i$  to construct a polyhedron of high dimension would lower the number of rounds needed to compute the solution.

Another avenue is to find better and faster preprocessing to minimize the problem.

## 5.2. Acknowledgments

This paper is written in grateful memory of the author's advisor Andreas Weber, who unexpectedly passed away recently.

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**Table 2**Comparison of run-times for SMTcut and PtCut sorted by ascending SMTcut run-time. Minimal runtimes are set in bold. Columns "BM", "Dim", "Comb", "PH", and "IntMaxPH" contain the BioModel number, dimension, theoretic number of combinations, number of polyhedra in the solution, and maximal intermediate polyhedra, respectively. A star in column "R" signifies a model with a rational vector field.

ВМ	R	Dim	Comb	PH	IntMaxPH	SMTcut	PtCut	Speed-up
26		10	$10^{14}$	6	32	0.1	0.1	1.0
397	*	10	$10^{8}$	0	_	0.1	14.9	101.6
30		16	$10^{22}$	6	48	0.2	0.3	1.7
41		11	$10^{10}$	4	924	0.2	1.4	6.8
491		36	$10^{6}$	1	1	0.3	17.2	66.6
492		18	$10^{9}$	1	1	0.3	2.9	9.1
28		22	$10^{10}$	17	119	0.4	0.4	1.0
482	*	23	$10^{26}$	17	495	0.6	2.3	4.1
637		16	$10^{25}$	12	1140	0.6	4.2	7.1
221	*	19	$10^{20}$	50	2573	0.7	2.1	3.1
21	*	33	$10^{84}$	46	3408	0.7	3.0	4.3
48	*	10	$10^{21}$	5	1160	0.8	29.2	38.1
315		13	$10^{14}$	13	432	0.8	2.5	3.3
599		24	$10^{23}$	24	456	1.6	5.8	3.6
328		17	$10^{23}$	86	140	1.7	1.4	0.8
22	*	67	$10^{38}$	147	1170	1.8	2.0	1.1
200		27	$10^{18}$	20	4704	2.2	64.0	29.7
666	*	22	$10^{16}$	64	464	2.2	5.6	2.6
489		24	$10^{16}$	42	4824	3.0	57.5	19.4
222	*	8	$10^{13}$	192	12516	3.1	11.0	3.5
638		8	$10^{15}$	13	2124	3.2	32.3	10.2
396	*	18	$10^{9}$	54	972	4.2	21.7	5.2
365		19	$10^{9}$	70	15030	4.3	583.7	134.2
147		30	$10^9$	54	5069	4.4	18.7	4.2
230		36	$10^{16}$	68	3330	5.1	24.6	4.8
498	^	50	$10^{17}$	214	1750	6.1	3.3	0.5
431		47	$10^{16}$	155	984	6.6	13.2	2.0
105		27	$10^{28}$ $10^{21}$	130	21088	9.7	644.2	66.5
102		27	$10^{21}$ $10^{11}$	322	4784	12.2	7.2	0.6
32		43	$10^{11}$ $10^{16}$	244	1092	12.8	110.0	8.6
407		23	$10^{24}$	212	15010	15.7	968.2	61.7
477		35	$10^{10}$	467	23460	33.8	571.0	16.9
576 93		57 52	$10^{25}$	756 596	10752 47772	48.6 55.3	55.8 6113.4	1.1 110.5
183		19	$10^{9}$	1	4///2	77.7	> 72000.0	> 926.4
501		35	$10^{25}$	916		102.8	> 72000.0	> 700.3
430		34	$10^{18}$	1676	4683	128.2	> /2000.0 58.0	0.5
103		30	$10^{16}$	1938	111402	224.9	763.5	3.4
74		12	$10^{12}$	9685	- 111402	941.5	> 72000.0	> 76.5
73		21	$10^{24}$	13449	_	1067.7	> 72000.0	> 67.4
61		34	$10^{27}$	10084	1784868	1661.3	26408.6	15.9
14		86	$10^{67}$	> 2663		> 7200.0	> 72000.0	-
151		66	$10^{44}$	> 7734	_	> 7200.0	> 72000.0	_
410		53	$10^{41}$	> 10612	_	> 7200.0	> 72000.0	_
560		59	$10^{29}$	> 10012	_	> 7200.0	> 72000.0	_
730	*	45	$10^{47}$	> 15310	_	> 7200.0	> 72000.0	_
, 50		10	-0			00.0	, _ 500.0	

**Table 3**Run-times in seconds without and with preprocessing for different models using the CVC4 solver, sorted ascending by number of polyhedra. Minimal times are in boldface. Column "PP time" contains the time for preprocessing and column "after PP" the run-time minus the preprocessing time.

ВМ	Dim	Comb	PH	No PP	With PP	PP time	After PP	Speed-up
397	10	108	0	0.1	0.5	0.5	0.0	0.29
183	19	$10^{9}$	1	77.7	2988.7	2988.7	0.0	0.03
491	36	$10^{6}$	1	0.3	3.4	3.4	0.0	0.08
492	18	$10^{9}$	1	0.3	3.4	3.4	0.0	0.09
41	11	$10^{10}$	4	0.2	2.6	2.6	0.1	0.08
48	10	$10^{21}$	5	0.8	29.8	29.6	0.2	0.03
26	10	$10^{14}$	6	0.1	0.9	0.8	0.1	0.14
30	16	$10^{22}$	6	0.2	2.7	2.6	0.1	0.07
637	16	$10^{25}$	12	0.6	5.3	5.0	0.3	0.11
315	13	$10^{14}$	13	0.8	9.3	8.9	0.4	0.08
638	8	$10^{15}$	13	3.2	54.9	54.2	0.8	0.06
28	22	$10^{10}$	17	0.4	2.5	2.0	0.4	0.18
482	23	$10^{26}$	17	0.6	2.8	2.5	0.4	0.20
200	27	$10^{18}$	20	2.2	29.2	28.3	0.9	0.07
599	24	$10^{23}$	24	1.6	9.7	8.4	1.2	0.17
489	24	$10^{16}$	42	3.0	59.9	57.6	2.3	0.05
21	33	$10^{84}$	46	0.7	2.2	1.6	0.6	0.31
221	19	$10^{20}$	50	0.7	2.9	2.3	0.6	0.24
147	30	$10^{9}$	54	4.4	20.8	18.1	2.7	0.21
396	18	$10^{9}$	54	4.2	20.6	18.3	2.3	0.20
666	22	$10^{16}$	64	2.2	4.8	2.7	2.1	0.45
230	36	$10^{16}$	68	5.1	49.6	44.4	5.2	0.10
365	19	$10^{9}$	70	4.3	13.6	10.8	2.8	0.32
328	17	$10^{23}$	86	1.7	3.5	1.8	1.7	0.49
105	27	$10^{28}$	130	9.7	93.1	85.6	7.5	0.10
22	67	$10^{38}$	147	1.8	3.7	1.8	2.0	0.48
431	47	$10^{16}$	155	6.6	18.2	11.8	6.4	0.36
222	8	$10^{13}$	192	3.1	6.7	3.7	3.0	0.47
407	23	$10^{16}$	212	15.7	27.4	10.9	16.5	0.57
498	50	$10^{17}$	214	6.1	8.6	3.2	5.4	0.71
32	43	$10^{11}$	244	12.8	17.4	5.8	11.6	0.74
102	27	$10^{21}$	322	12.2	25.7	15.7	10.0	0.48
477	35	$10^{24}$	467	33.8	26.5	5.6	20.8	1.28
93	52	$10^{25}$	596	55.3	86.2	39.0	47.2	0.64
576	57	$10^{10}$	756	48.6	62.0	20.0	42.0	0.78
501	35	$10^{25}$	916	102.8	87.0	13.2	73.9	1.18
430	34	$10^{18}$	1676	128.2	119.1	7.7	111.4	1.08
103	30	$10^{16}$	1938	224.9	589.2	422.2	167.0	0.38
74	12	$10^{12}$	9685	941.5	861.7	4.6	857.1	1.09
61	34	$10^{27}$	10084	1661.3	1579.5	139.5	1439.9	1.05
73	21	$10^{24}$	13449	1067.7	1024.0	5.0	1018.9	1.04

**Table 4**Relative run-time used for Searching another point, Minimizing a polyhedron and Inclusion checking for models that took more than one second to compute, sorted by ascending number of polytopes. The second part of the models did not finish and the numbers signify only the times until the process was terminated. The largest portion of time is set in boldface.

BM	PH	Time	% in S	% in M	% in I
183	1	77.7	91.7	4.3	0.1
638	13	3.2	63.6	27.1	1.3
200	20	2.2	52.8	35.9	1.5
599	24	1.6	28.0	56.2	3.0
489	42	3.0	31.6	55.2	2.9
147	54	4.4	34.2	53.3	2.9
396	54	4.2	19.1	62.5	6.3
666	64	2.2	16.9	60.2	6.8
230	68	5.1	33.5	53.3	4.4
365	70	4.3	31.3	55.0	3.5
328	86	1.7	16.9	56.8	5.7
105	130	9.7	43.7	45.8	3.1
22	147	1.8	19.1	45.4	5.8
431	155	6.6	22.3	60.2	6.0
222	192	3.1	27.6	40.6	7.2
407	212	15.7	13.8	67.2	11.9
498	214	6.1	19.4	53.2	12.1
32	244	12.8	11.6	62.2	17.2
102	322	12.2	26.9	51.9	8.9
477	467	33.8	9.0	51.9	30.5
93	596	55.3	15.7	64.3	13.3
576	756	48.6	12.7	60.1	19.7
501	916	102.8	11.5	68.2	15.5
430	1676	128.2	10.2	50.8	32.1
103	1938	224.9	27.5	54.5	12.6
74	9685	941.5	4.5	17.8	71.6
61	10084	1661.3	7.9	31.5	56.4
73	13449	1067.7	4.2	15.9	73.4
14	> 2663	> 7200.0	11.9	73.1	14.5
151	> 7734	> 7200.0	1.9	22.5	74.8
410	> 10612	> 7200.0	5.6	40.5	52.6
560	> 12577	> 7200.0	1.9	29.3	67.5
730	> 15310	> 7200.0	4.3	36.2	57.5