

# Method for measuring torques of electric motors using machine vision

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## Abstract

The object of research is the process of determining the angular displacement of dynamometric transmission mechanisms, which are used to measure the torques of electric motors. The paper analyzes methods of converting torques into a unified signal, taking into account destabilizing factors. Study of the accuracy of measurements during their application. In the course of the conducted research, various methods and means of measurement were considered, in particular, the use of tensometry and inductive transducers. It was found that such tools require periodic maintenance. In particular, mechanical transmission dynamometers measure torque by visual observation of angular deformation, which is converted into torque by visualizing the angle of rotation of the shaft using a Nonius angle scale. It is substantiated that such a measurement method has not left its relevance, because instead of involving an operator to determine the measurement results, it can be supplemented by using machine vision to determine the measurement results. And its application can find practical implementation in aggressive conditions, where electronic measuring transducers, due to aggressive conditions, cannot be used. In this regard, a method of measuring torques of electric motors based on machine vision is proposed. Its approbation was carried out using modeling tools and a specially developed prototype, based on which a tensometric-type measuring transducer with the possibility of visualizing the measured signal and its fixation by means of machine vision was proposed. A method of determining the measured value using known software and hardware solutions is proposed. The solution of similar tasks with the help of machine vision is discussed, taking into account the disadvantages caused by low speed and sensitivity.

## Keywords

torque, electric motor, measurement accuracy, measurement error, measuring device

## 1. Introduction

Ensuring the accuracy of measurements of dynamometric moments of electric motors in difficult conditions is one of the key tasks of metrological support. In contrast to the methods of measuring static moments, which are carried out with a stationary stator, it requires taking into account variable loads and rotation speeds, which places higher demands on the accuracy and speed of the characteristics of the measuring equipment. At the same time, it is possible to achieve high measurement accuracy only with the use of force-measuring sensors, which are placed directly on the shaft.

Considering the fact that modern technologies for the conversion of measurement information allow such measurements to be performed with high accuracy using tensometry, optical, inductive and capacitive methods, they require periodic maintenance, specific power conditions, special vibration filtering methods, etc.

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At the same time, torsion dynamometers have existed for quite some time, which allow you to visualize the twisting angle of the dynamometric element, which has a proportional relationship with the rotational load, using the Nonius scale. Thus, the angular deformation is transformed into a torque through the visualization of the twisting of the dynamometric element placed on the shaft. This traditional method is quite simple and reliable, but requires the participation of the operator. It can be used in aggressive environments where electronics cannot be used, especially when it comes to measuring directly on the motor shaft. In recent years, the relevance of such measuring instruments has increased due to the need to master environments where conventional electronics may be ineffective, such as radiation exposure, open space conditions, high pressure at great depths, and other extreme conditions. Therefore, there is a need to automate the measurement process while preserving the proven methodology. There is also the question of the need to improve outdated force measuring devices.

In such conditions, machine vision tools can be used to recognize the measurement results. However, this requires additional research into the speed, accuracy, sensitivity, and linearity of such solutions.

## 2. Literature review

The study of ways to identify measurable quantities using machine vision is becoming more and more popular. The main idea of using machine vision to determine torques is the analysis of the angular displacement of the shaft.

The methodology of identifying the movement of moving objects has long been used in various industries. For example, work [1] proposed a displacement estimation technique, which is used to determine the displacement of objects by integrating asynchronous acceleration measurements using a Kalman filter. An improved feature matching algorithm has been developed for better object tracking. This allowed combining asynchronous measurements with different sampling rates to improve displacement estimation. The effectiveness and practicality of the proposed method were confirmed by means of tests. In all tests, the proposed technique made it possible to accurately estimate displacement with an error of 3%.

The application of this technique to determine the angle of rotation of the shaft can be used with the use of special marks on the shaft. At the same time, the automatic determination of the scaling factor will be able to translate measurements from pixel units to angular units. However, such a method will be dependent on visual accessibility, prone to errors at high rotation speeds, sensitive to external influences, and requires complex calibration and system setup. May depend on lighting conditions and other external factors. In [2], a method of displacement measurement using the edge contrast enhancement (EEM) technique is proposed, which is a significant improvement compared to the previous orientation coding (OCM) technique. First of all, EEM improves the ability to track low-contrast objects, especially in low-light conditions. Unlike OCM, which uses image orientation gradients only, EEM also applies magnitude gradients, which allows for better highlighting and enhancement of subtle edge features. This significantly improves the ability to identify edges, which in turn increases tracking accuracy and reliability.

The main disadvantage of the EEM method is the high requirements for computing resources and processing time due to the complexity of the algorithms for detecting and enhancing fine edge characteristics, especially in conditions of low contrast and variable lighting.

Given the possible increase in error, adapting the method of identifying the angular displacements of the dynamometric elements of the measuring transducers can be quite appropriate in situations where the main priority is uninterrupted operation with minimal maintenance costs. In addition, there are quite simple solutions for the implementation of the system itself for recognizing the angular deformation of the dynamometric element of the shaft. For example, the method presented in this article can be applied on the basis of a cheap Raspberry Pi mini computer, the power of which, as shown by the research of this article [3], is sufficient to recognize moving objects by determining their spatial coordinates. This approach can be useful in areas where the accuracy of torque measurement is not high. But a more accurate measurement requires more computing power.

At the same time, it poses new challenges to developers, requiring constant improvement of both algorithmic and optical means of identifying moving objects. But there are approaches where, despite the low resolution of the camera and the processing speed of the video stream, the application of machine vision can be improved.

Thus, in work [4], Faster Region-Based Convolutional Neural Networks (Faster RCNN) machine learning models were used, which made it possible to identify and classify red and blue boxes by processing images obtained from a low-resolution camera on a Raspberry Pi 3 B+. This became possible thanks to deep learning algorithms, which are able to effectively analyze and recognize objects even with limited image quality. Experimental results demonstrated that even with limitations related to image quality, the system was able to achieve an accuracy of 78.8% in detecting and sorting red and blue boxes. Regarding the analysis of rotational motion, a number of limitations related to the speed of image processing should be highlighted.

In work [5], the problem of processing speed of rotary movement was solved by introducing additional signal labels into the design, which greatly facilitates the recognition of visual features of the object. Thus, the obtained results demonstrate that the proposed framework effectively solves the problem of image processing speed required for rotational motion analysis and can serve as a reliable platform for future applications. But at the same time, a significant number of destabilizing factors significantly reduces the accuracy of the measurement. Therefore, attention should be paid to the possibility of building a three-dimensional model of the electric motor shaft, and special marks of the dynamometric element can be recognized using detectors of special points, for example, SIFT. The experience of using this method can be taken from the article[6], where the determination of the position of objects was implemented using stereoscopic binoculars.

This approach can be adapted to measure torques, using the system's ability to accurately determine the spatial position and orientation of objects. The use of computational algorithms for image processing with recognition of SIFT detectors allows you to create accurate 3D models of rotating objects. This can be useful for monitoring and controlling torques in various engineering applications.

But this method cannot be used to determine the angular movements of the shaft under conditions of high speeds, since there is a need for additional recognition tools.

For example, in [7] a method of self-measuring the speed of the robot and controlling the torque of the electric motor is proposed. However, the methods proposed in the article do not take into account the risk of inaccuracies in speed and moment measurements, especially in conditions of variable loads or unstable power supply. Therefore, in control systems, especially those that depend on computational algorithms, there can be a delay between the measurement of speed and the corresponding adjustment of torque, which can affect the smoothness and accuracy of the robot's movement. From this example, you can take approaches to the synchronization of data from different sensors for accurate measurement of parameters in dynamic conditions, which allows you to accurately track the time and place of shooting. This can be adapted to monitor changes in shaft position in real time.

Gyroscopic methods, which also use visual cues of motion but do not focus on images, should also be considered. For example, methods of probe scanning of shaft movement are usually based on measuring the frequency characteristics of the set with various optical sensors, as well as resistive methods based on the proportionality of the shaft rotation angle and the illumination of the strain gauge receiver, which records the level of illumination intensity as a result of the angular movement of the dynamometric element. The principle of operation of such methods is described in works [8, 9, 10]. However, they have significant limitations related to the need for precise alignment of optical components and high sensitivity to external influences, such as light pollution and mechanical vibrations. This can significantly affect the accuracy and reliability of measurements.

An alternative to the already existing methods of measuring torques can be methods based on computer vision, which allow determining the angle of rotation of the shaft depending on the load moment [11, 12]. However, the main unsolved problem of the considered methods, which can be applied to estimate the rotational moment, is the difficulty with accurate determination of angular displacements in conditions of high rotation speeds and variable lighting conditions, which can lead to errors in measurements [13, 14, 15, 16, 17].

### **3. The purpose and objectives of the research**

The purpose of the study is to develop a method of measuring the torques of electric motors based on machine vision, which will make it possible to apply this method in conditions where conventional measuring transducers cannot be used.

To achieve the goal, the following tasks were set:

- develop a prototype of a dynamometric clutch that signals the level of rotational load on the electric motor shaft;
- propose a method of processing visual information that characterizes the measurement parameter.

### **4. Research materials and methods, object and research hypothesis**

The object of the research is the development of a method of measuring the torques of electric motors using machine vision. The research hypothesis suggests that the application of machine vision can be used in conditions where traditional measuring devices are ineffective.

This study involves the development of a prototype of a dynamometric clutch capable of recording the level of rotational load on the shaft of an electric motor, as well as the development of a method of processing the received visual information from this clutch.

It is assumed that the use of these approaches will reduce the problem of introducing machine vision into the process of measuring the dynamic characteristics of electric motors and will contribute to the further development of the accuracy and speed of this method, which can be used in particularly difficult conditions of operation of measuring devices [18, 19, 20, 21].

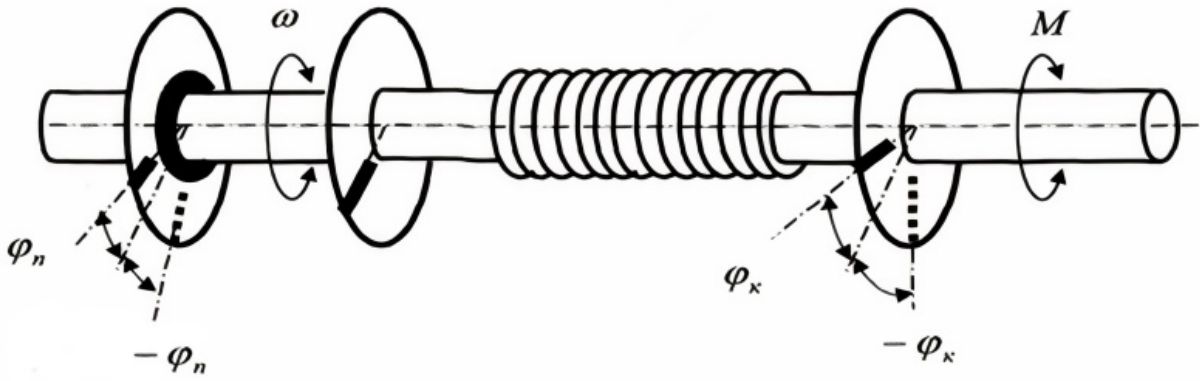
### **5. Requirements for the development of a dynamometric clutch that signals the level of rotational load on the shaft of an electric motor and a method of processing visual information from a dynamometric clutch**

The development of a prototype of a dynamometric clutch involves the creation of a device capable of measuring rotational loads on an electric motor shaft in real time. The design of the coupling includes sensors that can withstand mechanical loads and ensure the stability of measurements. The coupling is also equipped with an interface for easy integration with electric motor control systems and data transmission in digital format. The prototype must be tested for its ability to withstand long-term use in various operating modes of the electric motor, including maximum revolutions and load changes.

In parallel with the development of the coupling, the development of a method of processing visual information coming from the coupling is proposed. The processing system automatically analyzes visual information to determine measurement parameters [22, 23]. The development of a graphical user interface for visualization and analysis of measurement results in real time is also expected [24, 25, 26, 27, 28, 29, 30].

### **6. Development of a prototype for measuring the torque based on recognition of the angle of rotation of the shaft. Principle of operation**

The method that can be used to measure the rotational moment of an electric motor is based on the well-known principle of converting the elasticity of the dynamometric element into dynamic moment (Figure 1).



**Figure 1:** Structure of the dynamometric element for measuring the torque.

The angle of twist of two sections of the dynamometric element relative to each other can be represented by the expression:

$$d\mu = \frac{d_a d_\varphi}{\cos a}, \quad (1)$$

where  $d_a$  - infinitesimally small value by which the angle of inclination changes;  $d_\varphi$  length of sections perpendicular to the axis of the dynamometric element, the angle between which is minimal;  $a$  - angle of inclination of the helical line of the dynamometric element.

Taking into account the length of the dynamometric element, the twist angle can be determined as follows:

$$d\mu = \frac{dM dL}{GJ_0} = \frac{dPR \cos \alpha dL}{GJ_0}, \quad (2)$$

$$J_0 = \frac{\pi d^4}{32}, \quad (3)$$

$$dL = \frac{R d_\varphi}{\cos a}, \quad (4)$$

where  $L$  - length of the dynamometric element;  $dL$  - distance between two sections;  $R$  - radius of turns of the spring of the dynamometric element;  $J_0$  - moment of inertia of the cross-section of the spring relative to the center of this cross-section;  $dP$  - force acting at the moment of twisting the spring;  $d$  - diameter of the wire from which the spring of the dynamometric element is wound;  $G$  - shear modulus of the spring material;  $dM$  - twisting moment acting on the cross section of the spring  $dM = dPR \cos a$ .

Deformations  $\varepsilon_1$  and  $\varepsilon_2$  associated with deformations in the  $X$  and  $Y$  directions can be described by the following dependencies:

$$\varepsilon_1 = \frac{\varepsilon_x + \varepsilon_y}{2} + \frac{\varepsilon_x - \varepsilon_y}{2} \cos \theta_1 + \frac{\gamma_{xy}}{2} \sin \theta_1, \quad (5)$$

$$\varepsilon_2 = \frac{\varepsilon_x + \varepsilon_y}{2} + \frac{\varepsilon_x - \varepsilon_y}{2} \cos \theta_2 + \frac{\gamma_{xy}}{2} \sin \theta_2, \quad (6)$$

where  $\theta_1$  and  $\theta_2$  are the angles that determine the orientation of the axes relative to the main axes of deformation of the elastic element.

Hence, the shear deformations are expressed by the formula:

$$\gamma_{xy} = \frac{2(\varepsilon_1 - \varepsilon_2) - (\varepsilon_x - \varepsilon_y)(\cos \theta_1 - \cos \theta_2)}{\cos \theta_2 - \sin \theta_2}, \quad (7)$$

If  $\cos \theta_1 \equiv \cos \theta_2$ , then:

With:

$$\theta_1 + \alpha = -\pi/2, 0, \pi/2, \pi \dots \frac{n\pi}{2} = \theta_2 - \alpha, \quad (8)$$

The maximum angular twist of the dynamometric element will have the expression:

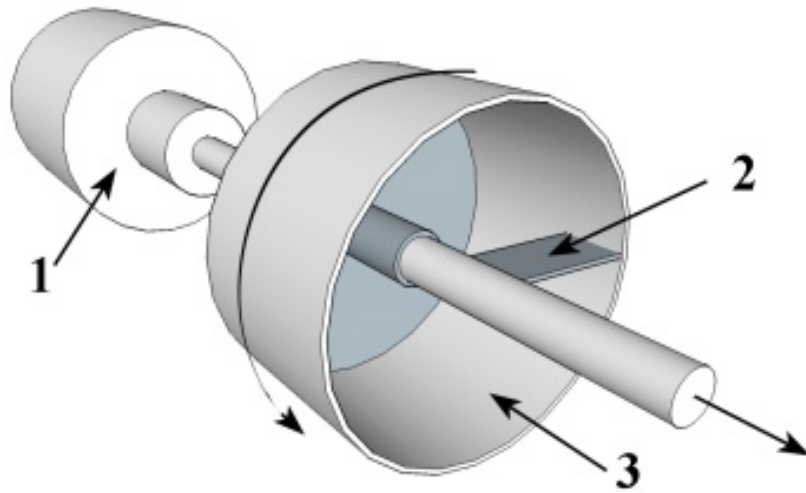
$$\gamma_{MAX} = \sqrt{\gamma_A^2 + \gamma_B^2}, \quad (9)$$

Using the Mohr diagram, the main deformations can be calculated as follows:

$$\varepsilon_p, \varepsilon_q = \frac{\varepsilon_1 - \varepsilon_3}{2} \pm \frac{1}{\sqrt{2}} \sqrt{(\varepsilon_1 - \varepsilon_2)^2 + (\varepsilon_2 - \varepsilon_3)^2}, \quad (10)$$

At the same time, determining the dependences of dynamometric elements on the shaft twist angle can be complicated by difficulties in setting up and calibrating such a system. Therefore, to determine the rotational force, it is possible to use a strain gauge sensor, which has greater sensitivity and known grading characteristics.

In this case, the structure of the measuring transducer will have the following form (Figure 2).



**Figure 2:** Tensometric method of measuring torque.

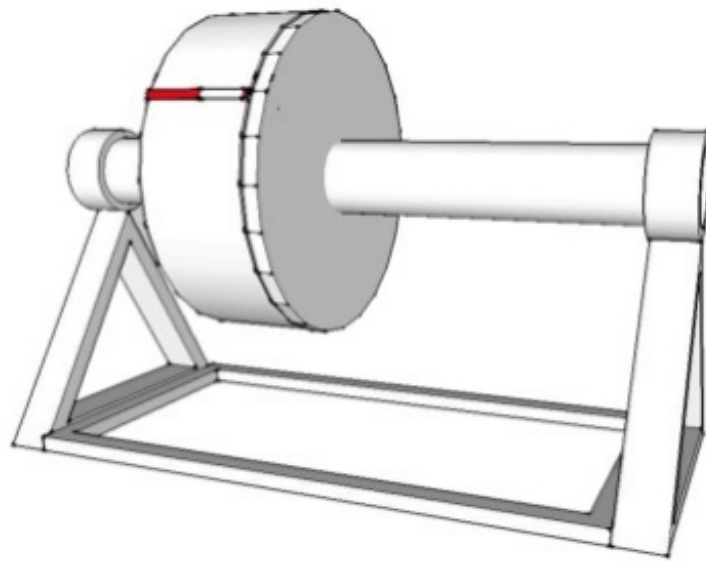
Designation in Figure 2: 1 is an electric motor; 2 – rigidly fixed strain gauge sensor to the body of the strain gauge coupling; 3 – strain gauge clutch, which is connected to the electric motor shaft through strain gauge sensor 2.

Based on this, a prototype of a dynamometric coupling for measuring torque (Figure 3) is proposed, which consists of an AS5600 angular displacement sensor (Figure 4), a strain gauge sensor (Figure 5), which is built on the basis of an HX711 microcircuit, which converts an analog signal received from a strain gauge bridge, which housed in an aluminum case measuring 75x12.7x12.7 mm. Allows you to convert deformation into an electrical signal, supporting a maximum load of up to 1 kg.

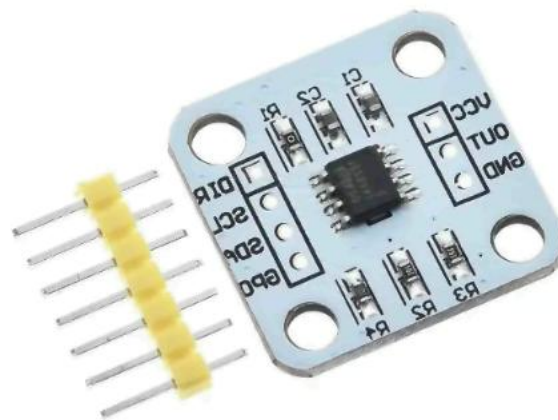
As well as an electrical circuit for determining the level of the sensor's output signal, which is built on the basis of the LM3914 integrated circuit (Figure ??), which allows you to convert the output signal of the microcircuit into a qualitative indicator of the measured signal.

Thus, the measurement of the torque is based on the conversion of the mechanical load into an analog signal using a strain gauge bridge. This primary signal is fed to an analog-to-digital converter (ADC), which processes and converts it into digital form. Further processing of the signal is carried out using the HX711 chip, which forms a unified output signal. This signal is fed to the LM3914 chip, which allows visualization of the shaft load level using an indicator, thereby providing the ability to determine the shaft load in real time [31, 32, 33, 34, 35, 36].

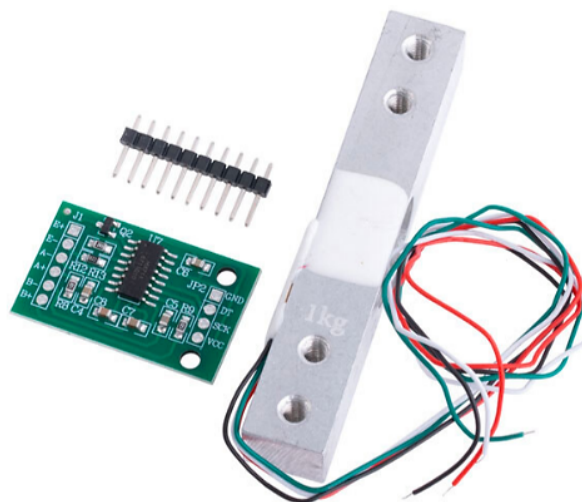




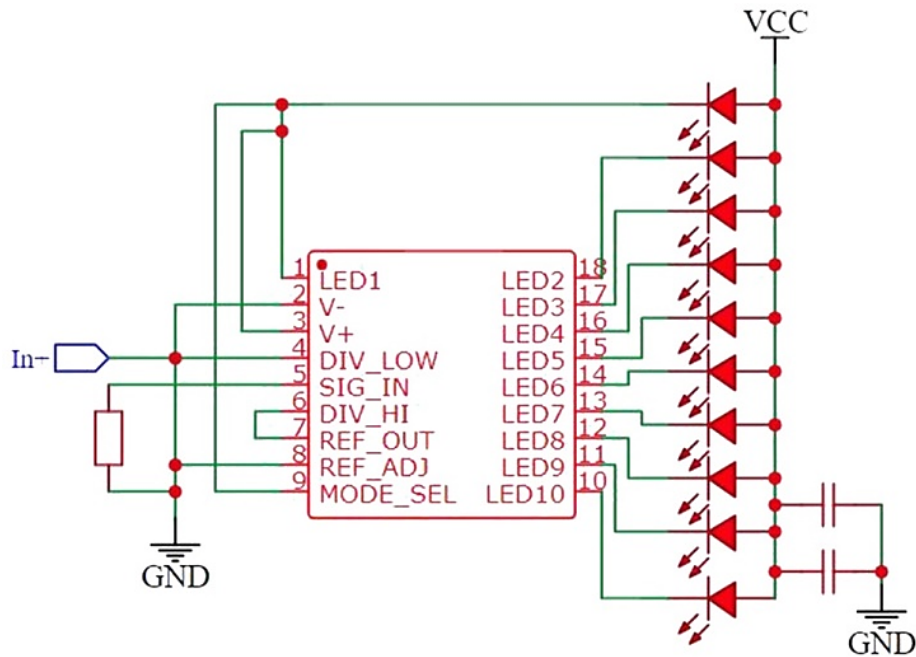
**Figure 3:** Measuring dynamometric clutch.



**Figure 4:** Sensor of angular movements AS5600.



**Figure 5:** Strain gauge sensor.



**Figure 6:** Circuit diagram for converting the output analog signal of the AS5600 sensor into a visual indication of its level. Built on the basis of the LM 3914 microcircuit

## 7. A method of recognizing a change in a signal indicator using machine vision

Considering the display of the signal level as a scale placed in the form of an LED matrix on the housing of the dynamometric coupling (Figure 3), it is possible to compile the program code for identifying the signal level by setting a virtual scale:

```
import cv2
import numpy as np

# Load the image using OpenCV
image = cv2.imread(patch)

# Convert image to HSV color space to detect red color more accurately
hsv_image = cv2.cvtColor(image, cv2.COLOR_BGR2HSV)

# Define range for red color in HSV
lower_red = np.array([0, 120, 70])
upper_red = np.array([10, 255, 255])
lower_red2 = np.array([170, 120, 70])
upper_red2 = np.array([180, 255, 255])
light_red = np.array([160, 100, 100])
dark_red = np.array([180, 255, 255])

# Create masks for red color
mask1 = cv2.inRange(hsv_image, lower_red, upper_red)
mask2 = cv2.inRange(hsv_image, lower_red2, upper_red2)
mask3 = cv2.inRange(hsv_image, light_red, dark_red)
combined_mask = mask1 + mask2 + mask3

# Find contours in the mask
contours, hierarchy = cv2.findContours(combined_mask, cv2.RETR_EXTERNAL, cv2.CHAIN_APPROX_SIMPLE)[-2:]
```



```

# Initialize list to hold the x-coordinates of indicator and reference lines.
line_x_coords = []

# Loop through the contours to find the x-coordinates.
for contour in contours:
    # Get the bounding box of the contour.
    x, y, w, h = cv2.boundingRect(contour)
    # Store the x-coordinate of the center of the bounding box.
    line_x_coords.append((x + x + w) // 2)

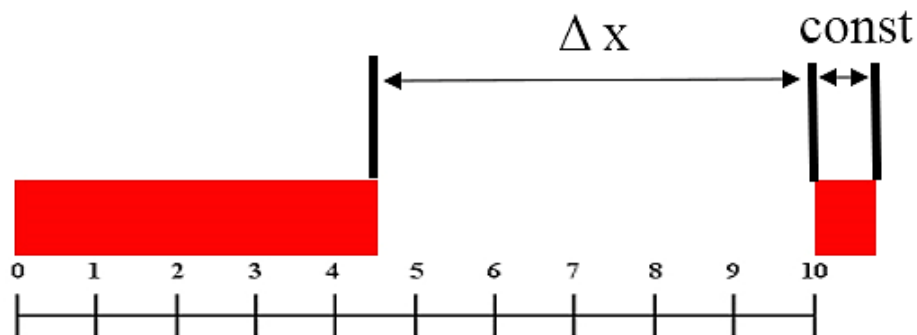
# Sort the x-coordinates
line_x_coords = sorted(line_x_coords)

# Assuming the leftmost line is the indicator and the rightmost line is the reference
# Check if we have at least two lines detected
if len(line_x_coords) >= 2:
    indicator_x = line_x_coords[0]
    reference_x = line_x_coords[-1]
    # Assuming the reference line (rightmost) is at position 10 Nm, we scale the
    # measurement accordingly
    scale_factor = 10 / (reference_x - indicator_x)
    # Now we measure the distance of the indicator line from the 0 position, scale it,
    # and that's our measurement
    measurement = (indicator_x - line_x_coords[0]) * scale_factor
else:
    measurement = None

measurement, indicator_x, reference_x

```

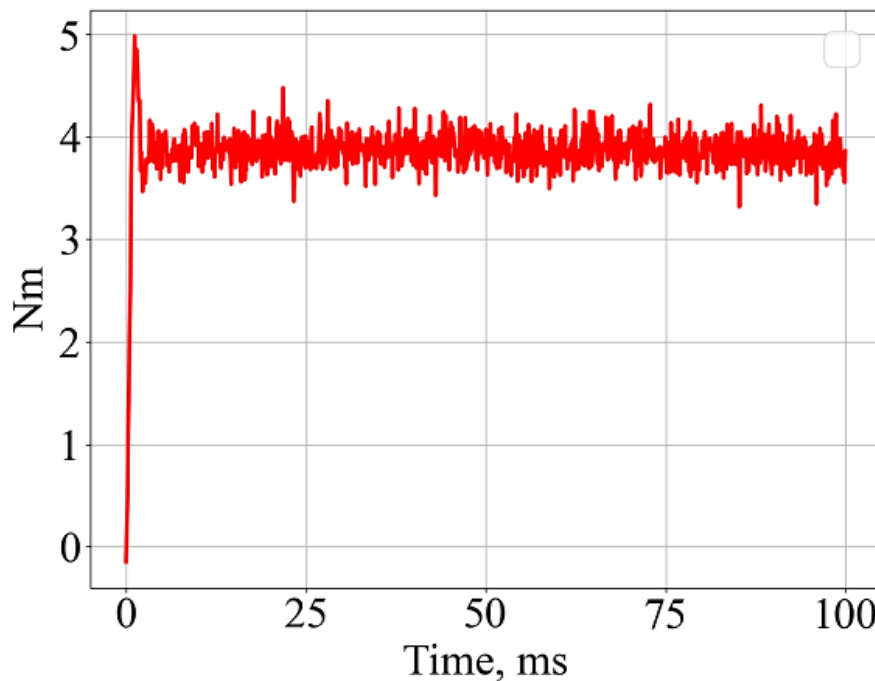
As part of this code, the image is first loaded using OpenCV library functions. For better identification of red elements in the image, it is converted from the standard BGR color space to the HSV model. This allows you to more accurately determine the ranges of red color, in particular for its various shades. Next, color masks are created that highlight red areas in the image. The program uses these masks to find the contours corresponding to the red lines. Each contour found is analyzed and a central x-coordinate is determined for it. After finding all the x-coordinates, they are sorted to select the extreme points that represent the left and right red lines on the scale. The left line is a moment indicator, and the right line is a standard that remains unchanged and corresponds to the maximum value of the measurement (Figure 7).



**Figure 7:** Placement of signal and reference labels.

The program determines the scale factor by dividing the distance between the indicator and the standard by the known maximum value of the scale. Finally, it measures the torque using the location of the indicator line and converts it to a scale of 0 to 10 Nm. Testing of this method with the use of a

direct current electric motor made it possible to obtain the following results (Figure 8).



**Figure 8:** The result of torque measurement using machine vision.

Statistical observation of the measurement results showed a standard deviation of 0.22 in the stabilized operating mode. The relative error was 20%. So, this method of determining the loads on the shaft using machine vision and the proposed dynamometric clutch allowed to obtain the characteristics of the load intensity in a non-contact way. The use of the developed software code made it possible to conduct a comparative analysis of pixels on the signal and reference mark of the dynamometric clutch.

## **8. Discussion of the results of the assessment of the accuracy of measurements of dynamic moments and angular accelerations of electric motors**

The results of testing the method of determining torques on the shaft of a direct current electric motor using machine vision demonstrate the significant prospects of this technology for non-contact measurement. With the help of a specially developed dynamometric coupling, measurements were obtained, which are supported by statistical data. The standard deviation in the stabilized operating mode was 0.22, which indicates a fairly high stability of the measurement process. The relative measurement error was 25%, which indicates potential areas for further improvement of the technique.

The application of the developed software code for the comparative analysis of pixels on the signal and reference markings of the dynamometer coupling made it possible to analyze the load intensity in more detail. This made it possible to obtain more accurate data on the distribution of loads, which contributes to a better understanding of the behavior of the electric motor in various operating conditions.

Considering the obtained results, the method of using machine vision together with the dynamometric coupling proved to be effective for measuring torques. However, it should be noted that in order to achieve greater accuracy and reduce the relative error, it is necessary to optimize both the image processing algorithms and the physical components of the measurement system. Further research should focus on improving these aspects in order to reduce errors and improve measurement reliability.

## 9. Conclusions

The proposed method of measuring torque uses the capabilities of machine vision, which greatly simplifies traditional measurement methods. Testing of the method confirmed the possibility of its use for non-contact measurement of torques. The use of a specially developed dynamometric coupling ensured the stability of measurements with a standard deviation of 0.22. However, taking into account the complex cycle of transformations of the measured value, the relative error was 25%. Although this method does not provide high measurement accuracy, it can be applied in conditions where it is necessary to use visual data to obtain measurement information, in particular in those situations where traditional measuring equipment is unsuitable or cannot be applied.

## Declaration on Generative AI

The authors have not employed any Generative AI tools.

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